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Date: April 3, 2020

Subject: Implementation II

The SAE Mini Baja project is an international collegiate competition that requires a team of students to design and build a single-seat, all-terrain vehicle. The team will then compete with other collegiate design teams in a series of static and dynamic challenges. Northern Arizona University (NAU) possesses a team of 12 students to compete in the prestigious competition. The team is divided into four sub teams: Front End, Rear End, Frame, and Drivetrain. In the last month, the NAU competition team, Lumberjack Motorsports, has made major progress towards completing the manufacture of their vehicle. Milestones include the completion of suspension components, frame mounting configurations, and critical drivetrain components.

1 Implementation – Weeks 7-11

The following describes progress made by each sub team toward completing their system of the vehicle. Each sub team has been implementing their designs by fabricating components of their respective system, as well as assisting other sub teams in their manufacturing needs.

1.1 Manufacturing

The following section provides a brief description of the manufacturing processes implemented by the team to produce a complete final product.

1.1.1 Front End

The front-end sub team worked on manufacturing the control arms, cross bars for the upper control arms, mounting tabs and shock mounts designed to support the shock absorber. The cross bars were manufactured using 1" OD x 0.065" wall thickness 4130 Chromoly Steel tubing, which were cut to length using the chop saw in building 98C. The ends of the cross bar were subsequently coped using a drill and 1" OD hole saw bit from the machine shop in building 98C. The corresponding shock absorber and control arm mounting tabs were outsourced to Wicked Welding and Fabrication to be plasma cut. All mounting tabs were welded to the control arms and frame once they were received.

The control arms were manufactured in house by the team. A 1" OD x 0.065" 4130 Chromoly steel was used and it was cut to size, bent with the hydraulic bender and then scalloped for welding to the central uni-ball bearing. They team then fabricated chassis tube inserts on the lathe so the heim joints could be fitted into them and mounted to the mounting brackets. The team fitted and tacked the mounting avocados to every location of the front end where needed. Then once everything was tacked or welded together the front-end control arm assembly was mounted together completing the front suspension. All that remains is to bolt the shock absorbers into the mounts and the team will have fully functional front suspension.

The steering system had to be mounted on a steel plate that could hold the torsional and axial forces of the steering rack. A 1/8 in plate was used to mount the rack and instead of heim joints at the ends of the rack shaft clevis joints were manufactured in house. The clevis joints were manufactured with a 3/8 bolt that could fasten a 7/16 heim through it.

Low carbon steel was sourced from building 98C and cut to the dimensions of the rear brake rotor using the vertical bandsaw. This component was plasma cut by Wicked Welding and Fabrication due to geometry and material requirements. In addition to geometry requirements, the front brake rotors and supporting brake caliper mounts were laser cut by Vroom Engineering because the campus machine shop did not carry additional 1/8" or 3/16" thick low carbon steel required for manufacturing. The existing brake caliper mounting tabs on the aftermarket steering knuckle and the brake rotor mounting studs were cut short using an angle grinder to accommodate the brake caliper mounting bracket and brake rotor designs. This also allowed the front CV axles to be sleeved and installed to the front suspension for alignment verification.

1.1.2 Rear End

In the last month the rear end team has turned focus to assembling the parts manufactured to date. The parts being brought together include Trailing arm tubing, face plates, bearing housings, shock mounts, rear links, and ball joints. The face plates utilized the Tormach CNC machines in building 98c to create a space for the bearing to fit as well as lighten the plates. The bearing housings had to be cut using the horizontal band saw to get the length proper. The bearing housings were then put onto the manual lathe to be turned down to size and then a boring operation to get the inner diameter to proper size. The bearings could then be press fit into the housings using proper interference. The rear links were manufactured using the lathe to drill and tap to a 3/8 UNF left and right hand threaded. With all of these manufactured the assembly by welding the parts together began. The team was able to get two trailing arms built before spring break and aligned everything in preparation for shock mounts.

1.1.3 Frame

Since the frame had already been CNC bent and notched, all we had to do is weld the tubes together. This was done by Tyler Trebilcock since he is our designated certified welder for the project. Most of the frame was tacked together and some parts finish welded to make sure it was sturdy while we worked on the rest of the Baja. For the miscellaneous brackets such as the fire extinguisher tabs, the rule book was consulted to ensure rules were met and then the brackets were either CNC plasma cut for precise or complex parts, or simply cut by angle grinder out of the appropriate thickness plate steel. These were then tack welded onto the frame with their counterpart components to align them according to the SolidWorks models. Some tabs (such as body panel rivet tabs) were left over from previous Baja projects.

1.1.4 Drivetrain

The Drivetrain team has used several manufacturing processes during the implementation of the team's final product. Since the completion of mounting both differentials, several subsystems have seen progress. The gearbox has a completed aluminum case built using a CNC mill machine (through NAU campus machine shop), a completed gear mesh using outsourced fabrication in the form of wire EDM cutting (through AZ Wire Specialists) and carburized heat treatment (through Phoenix Heat Treating), as well as completed mounting hardware and brackets made through use of a drill press, an angle grinder cutting wheel and stationary grinding wheel (through NAU campus machine shop). The ECVT has seen significant progress, as the on-board computer was completed using a 3D printer, soldering, drilling, and. In the case of the mounting brackets, cutting, filing, and welding (through Jacob Najmy's personal equipment and NAU campus machine shop). The CV axles are in the planned process of fitment by cutting and replacing the original main shafts with hollow tubing (1.00" OD, 0.065" WT) of identical thickness to the driveshaft.

1.2 Design Changes -Weeks 7-11

The following section provides descriptions of design changes made to systems based on physical obstacles that occurred during manufacturing processes.

1.2.1 Front End

1.2.1.1 Design Iteration 1: Change in Brake Rotor Mounts discussion

One of the primary issues for the braking system of the vehicle was manufacturing mounts for the brake rotors and calipers. Because the rear brake rotor was required to be mounted on the rear CV axle, mounting tabs had to be placed on the shoulder of the CV axle and be short enough to avoid interfering with the contact surface of the rotor. The mounting tab was designed to feature a base with the same radius as the collar of the CV axle, and a top edge with the same radius as the inner radius of the rear rotor. Four tabs are equally spaced apart on the collar and welded in place to accommodate the PCD of the rear rotor. Figure 1 displays the proposed rear rotor mounting tab design.

Figure 1: Rear Brake Rotor Mounting Tab Design

In addition, the front brake rotors and calipers were required be mounted to the aftermarket hubs and steering knuckles without interfering with other components as the front axles rotated. As mentioned previously, the rotor mounting studs on the front hub were cut 0.5" shorter using an angle grinder to provide sufficient space between the brake rotor and steering knuckle. The existing mounting points for the brake caliper on the steering knuckle were cut 1" shorter to provide clearance for the brake caliper mounting bracket. Figures 2 and 3 display the knuckle and hub modifications, respectively. Figure 4 represents the front brake caliper mounting bracket design.

Figure 2: Brake Caliper Mounting Points - Original (left) vs Shortened (right)

Figure 3: Front Hub Assembly on CV Axle

Figure 4: Front Brake Caliper Mounting Bracket (Prototype)

1.2.2 Rear End

1.2.2.1 Design Iteration 1: Change in [subsystem/component] discussion

At the end of week before spring break the team assembled the parts of the trailing arm they had in place. At this point the team was able to visualize where the shocks would best align to not bind during use. The original plan of mounting was not able to be used as the shocks were too long, thus we moved it to more align. The plan for creating shock mounts can be seen in Figure 5, where the mounting points are circled. The original design was to have the mounts further up the trailing arm. The shocks were too short as well as the tire was rubbing on the shock mount. The old trailing arm can be seen attached to a previous year's frame in Figure 6.

Figure 5: Rear end shock mount locations

Figure 6: Old rear end shock mount

1.2.3 Frame

1.2.3.1 Design Iteration 1: Change in frame width discussion

In the process of welding the frame tubes together, there was a miscommunication on the width of the roll hoop being welded to the roll hoop lateral member. We accidentally welded it 1 inch wider overall. This caused very minor problems in other areas, but the CAD had to be updated to reflect the changes in order to model further mounting brackets that depended on this change. This change can be seen in Figure 7

Figure 7: CAD Model Differences

1.2.3.2 Design Iteration 2: Change in seat discussion

Once we started getting the cockpit are dialed in, we realized that the drive shaft under the seat was in fact hitting the seat. We checked the rule book on the height requirements with a driver in the seat. It in fact could not move up any further due to this restriction. Since the seat was molded off a school chair, the bottom was a simple shallow bowl shape. To make the small clearance we needed we cut out an oval shape along the drive shaft length. A thin sheet of aluminum was then bent to match the oval cut out and curved around the drive shaft. The seat was then taken to Nova Kinetics where we patched the hole with carbon fiber in the form of the bent plate. The logic behind this was that it would be just enough to clear the driveshaft and the seat might conform to a butt shape a little better. This ended up working perfectly for our needs. The before and during patching photos can be seen in Figure 8.

Figure 8: Seat Differences

1.2.4 Drivetrain

1.2.4.1 Design Iteration 1: Change in ECVT Shaft discussion

The engine output shaft connects to the first subsystem of drivetrain, which is the electric continuously variable transmission (ECVT). The ECVT has a custom sleeve that slides over the engine shaft that helps transmit torque to the sheaves. This is one of the most critical components in the drivetrain subsystem. After the design was finalized the team was ready to begin manufacturing. After discussion with the NAU shop employees the design was too complex for them to design. It required an effort of work they did not want to contribute. This led to further discussions of where to have the shaft manufactured. After talking with a local shop about manufacturing, the technician requested a redesign.

The redesigned shaft was designed for ease of manufacturing. This included a shorter shaft that allowed for bearings to be pressed in right next to each other. This still allowed the shaft to keep the contact points required for proper support but also allows for in house manufacturing. Figure 9 is the old shaft, which required complex manufacturing. Figure 10 is the new simple shaft, which still allows for support through bearings next to each other, while allowing for simple manufacturing.

Figure 9: Old Complex Shaft Design

Figure 10: New Simple Shaft Design

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2 Standards, Codes, and Regulations

The following section provides the standards that the team followed in their design and fabrication of the Baja in a table format.

2.1 Standards applied to project

For this project, we made sure to follow any standards set forth by the competition rule book along with any standards that applied to the parts being designed. This includes ASTM, ASME, ANSI, AGMA, AWS, ABMA, IEEE, NSPE, and SAE standards. Some standards did not apply directly to the design and manufacturing but to the project, such as using IEEE formatting in documentation.

3 Risk Analysis and Mitigation

The sub teams focused their respective designs to target potential failures identified through FMEA analysis. To ensure full mitigation of potential risks, sub teams often worked in collaboration, or simply mitigated risk by natural progression of individual designs.

3.1 Potential Failures Identified Fall Semester

The following section exhibits the potential failures most likely to occur in both the Front & Rear End and the Frame & Drivetrain systems. The ten most likely failures were selected based on RPN values. For a full list of potential failures, see Appendix 4.

3.1.1 Front & Rear End

Based on the full FMEA performed and provided in the appendix, the top ten main failure modes of the front and rear end subsystems are described below. Table 2 illustrates the top ten failures from the FMEA performed.

TADIC 2. LIST OF FTOIR LIIU AIRU INCAT LIIU CHRICAI TAHULGS													
Part # and Functions	Potential Failure Mode	Potential Effect(s) of Failure	Potential Causes and Mechanisms of Failure RPN		Recommended Action								
	Brake System Brake line leak or rupture	Decreased deceleration, brake system failure	Sharp cuts on the brake lines		480 Stainless steel Brake lines to resist abrasion, expansion								
Control Arms Weld failure		Complete control arm failure, arm component separation	Lack of material at weld joint		480 Ensuring all welds are strong through testing								
Steering	Deformation of teeth on pinion	Ineffective steering operation.	Over exerting torsion in a short time		480 Use durable material for rack and pinion								
	Brake System Master cylinder leak	Decreased braking system pressure, pedal will not retract	manufacturer defect, improper installation		400 Integrated master cylinder								
	Brake System Broken Calliper bracket	Loss of braking due to brake caliper movement	Impact/improper material selection		400 Use robust, durable metals and check routinely								
Control Arms	Tube failure	Complete control arm failure	Improper tubing calculations		400 Thick enough wall on tubing								
Steering	Quick release system detaches	Driver unable to control vehicle	improper installation/ mechanism failure		400 Use Ball-Lock guick release system								
CV Axles	Spline failure	No power to the wheel	Improper material selection		360 Ensure power through CV axle is appropriate splines								
	Brake System Brake pedal falls off	difficulty or loss of braking	improper installation/ manufacturing		360 Use a durable mount for pedal								
Roll Hoop	hraake frog from frame	loss of dampening frame bottoms out on obstacles	Susnansion bottoms out object strikes roll be		360 I lee durable metal and test welds								

Table 2: List of Front End and Rear End critical failures

The design changes did not affect the FMEA performed on the subsystems.

3.1.2 Frame & Drivetrain

The following table represents the top ten most likely failures anticipated to occur during the operation of the frame and drivetrain systems.

Part#and Functions	Potential Failure Mode	Potential Effect(s) of Failure	Severit y(S)	Potential Causes and Mechanism s of Failure	Occurrenc e(0)	Current Design Controls	Detectio n(D)	RP N
Frame contain and protect driver while holding together all other subcomponents together	Fatigue failure	broken members leading to unfunctional parts of the frame or entire Baja	8	repeated high stress situation	7	Over design the frame	9	504
ECVT modulates and transmits power from the	stepper motor overheatin g	ECVT would be stuck in gear	7	improper cooling	τ	ensure proper cooling is designed	7	343
engine to the gear reducer	electrical shortage	ECVT would be stuck in gear	6	improper soldering	6	use quality soldering techniques	9	324

Table 3: Frame & Drivetrain - Top Ten Critical Failures

No new potential failures were recorded in the frame and drivetrain systems.

3.2 Risk Mitigation

The following section provides short descriptions of design solutions to potential failures for each major system of the vehicle. Obviously, design solutions focus on the most likely failure scenarios, as seen in Section 3.1. For a full list of potential failures, refer to Appendix 4.

3.2.1 Front End

The Front End conducted several FEA analyses to determine the optimal geometry and material for suspension, steering, and brake components as well as mounting tabs for all subsystems. These analyses proved beneficial in the material selection and component design process, as the primary objective was to mitigate component failure due to stress. Due to the proper FEA analysis from the front-end team, the nose section of the Baja vehicle will perform well in the dynamic competitions.

Rear End

Rear End has implemented many design changes based on the risks and potential failures involved. One early design change the team focused on was reducing parts and eliminating the need for a knuckle. After running FEA on our trailing arm and testing the prototype, it was proven the design was certainly strong enough. We were worried about potential shocks not working correctly which was compensated for in the design for the brackets. The main concern was focused around the connecting ball joint from the trailing arm to the frame so the team made sure to use a thick enough material to be sure it can withstand the forces needed.

3.2.2 Frame

Since the frame only had one major potential failure mode it was not too difficult to mitigate that risk. This failure mode was fatigue failure. In the FMEA the RPN score was high since this failure would most likely be catastrophic, fatiguing happens all the time, and it is difficult to detect before failure. But that does not mean it is hard to mitigate. By leaning towards thicker and stronger materials when these decisions were made, this greatly reduced the risk of this kind of failure. One example of this is using chromoly steel instead of mild steel. This however made the frame more expensive. When components were made thicker, this also made the frame heavier than it otherwise would have been. While also reducing this risk we also helped mitigate many of our other failure modes. Many of them were variations

of different impacts which are helped by stronger and thicker materials.

3.2.3 Drivetrain

The Drivetrain team designed their system to mitigate the failures listed in Table 3 largely through collaboration with the Frame team. Many of the identified potential failures can be avoided using body paneling, as the primary function of paneling is to prevent penetration from external sources. The benefit of the paneling's function is that the risk of puncture to the gearbox and differentials is nearly nonexistent. Likewise, overheating in the gearbox and differentials are easily avoided through use of specified gear oils. For the differentials, SAE grade 80w-90 gear oil is the manufacturer suggested usable oil for the hardened steel gear mesh and is the industry standard for heavy duty gear mesh applications. For the custom-designed gearbox, a similarly weighted gear oil is used (75w-80), chosen for its lighter weight in cold conditions. The modification will allow for the gearbox to actuate easier during startup by providing less strain on the ECVT transmission system. Unfortunately, by using lighter weight oil in the gearbox, more strain can potentially occur in the differentials under cold conditions. The ECVT system itself is designed to mitigate overheating by incorporating more fans than originally included. More fans will provide increased airflow through the computing system to cool components by convection cooling at the cost of increased weight due to additional components. Electrical shortages in the system are mitigated by soldering techniques verified through multiple team members collaborating on both the soldering process and the testing of individual connections.

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4 Appendix 4.1 Front & Rear End Full FMEA

Table 4.1: Front & Rear End FMEA

4.2 Frame & Drivetrain Full FMEA

Table 4.2: Frame & Drivetrain FMEA

